# KRUSTY Integral Experiments, Modeling & Stability

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Jeffery Goettee, James Jurney, Robert Kimpland & Steven Klein

Los Alamos National Laboratory

**Advanced Nuclear Technology Group (NEN-2)** 

Manufacturing Science & Engineering (MET-2)

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## **Purpose**

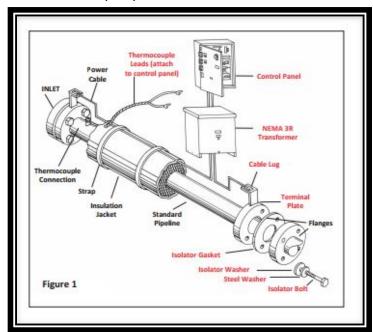
- Refine predicted performance through integral experiments focused on reducing uncertainties in parameters
  - Reactivity coefficients and cross sections of fuel, BeO reflectors, vessels, and other components across operating temperature range
  - Temperature and mechanical response of components as function of core temperature
  - Thermal reactivity feedback of core, reflector and cooling mechanisms
  - Sensitivity of performance to physical parameters and configuration
  - Dynamics including start-up and off-normal events
- Refine dynamic models as experimental data becomes available
  - Verify and ultimately validate predicted steady-state operation
  - Estimate system response to dynamic events such as start-up and off-normal events
  - Demonstrate theoretical stability of the system

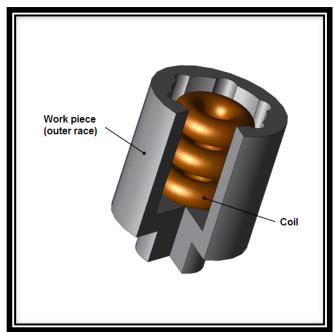


# **Experimental Campaign – Core Heating**

#### Core heating (impedance or inductive)

- Impedance method supplies electric current directly to uranium core; would be mounted in hollow center of the core; through vacuum vessel electrodes; power controller supply for required seven (7) kilowatts to heat to 800°C (1472°F)
- Inductance heating through coupled energy through hollow center; efficiencies require eleven (11) kilowatts to heat.







**Impedance Concept** 

**Inductance Concept** 

## **Core Heating – Examples**

Many configurations possible

Support of manufacturing and experimental





operations

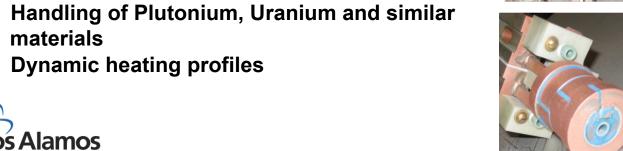


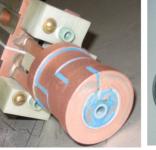








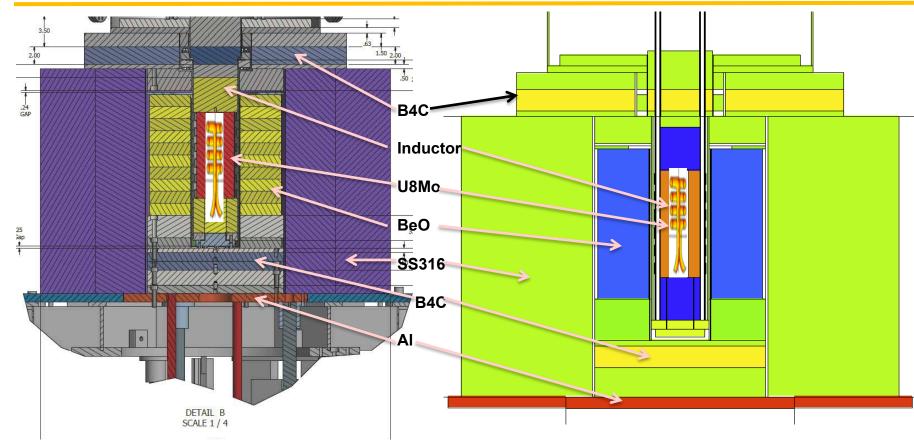








# **Zero-Power Critical Experimental Concept**



- Establish Zero Power throughout operating temperature range (20°C 800°C)
- No vessel, heat pipes or other structures required
- Potential for smaller scale experiments involving only BeO

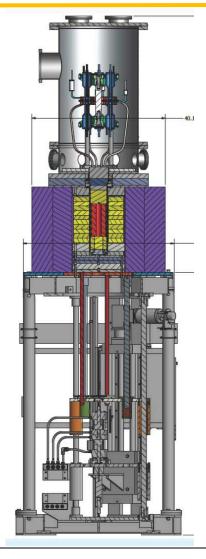




# **Critical Experiments – Full Configuration**

## Mounted on Comet Critical Assembly

- Repeat zero-power experiments with sub-critical heating to examine system performance
- Perform selected off-normal events
- Repeat temperature profile at power







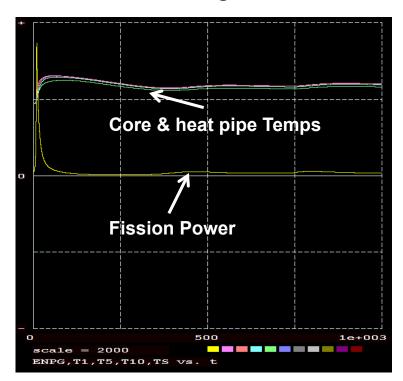
## Critical Experiments – Safety, Security & Operational Issues

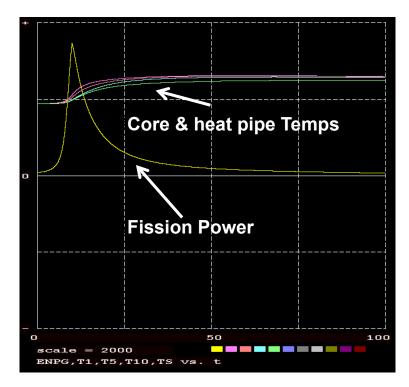
- 72 hours continuous operation
- Excess reactivity (~\$3.00 versus current \$0.80 limit)
- Operations with vacuum chamber
  - Determination of preoperational checks
  - Monitoring requirements
  - Actions arising from breach
- Temperature of operation
  - Monitoring requirements
  - Limits
- Handling and disposition of fission gasses
  - Exhaust or trap? (Environmental Impact Statement determination)
  - If exhaust determine operational mode of HVAC system
- Effects of reflector cooling, material sweep, and potential HEPA filtration



# **Dynamic System Simulation (DSS)**

- Coupled nuclear kinetics and thermo-hydraulics with expected reactivity feedback
- Startup, transition to steady-state and off normal events modeled
- Current model uses generic heat transfer mechanism



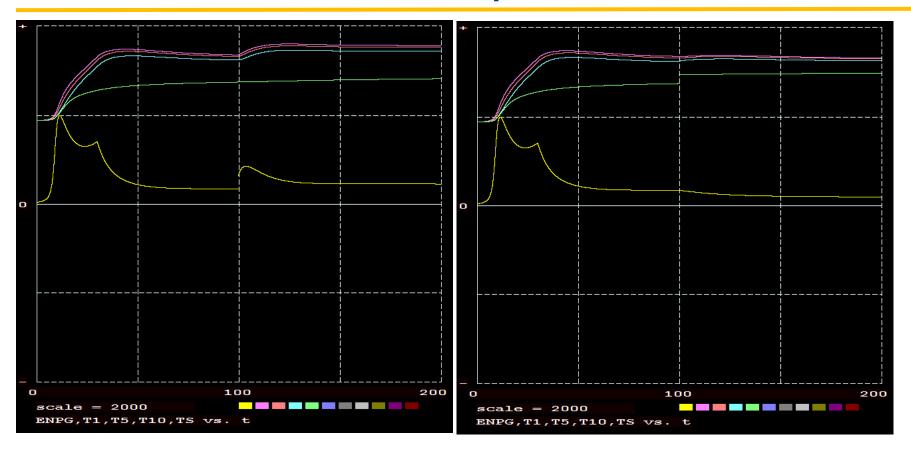




\$1.00 insertion (Detail)



# **DSS with Off-Normal Event Response**

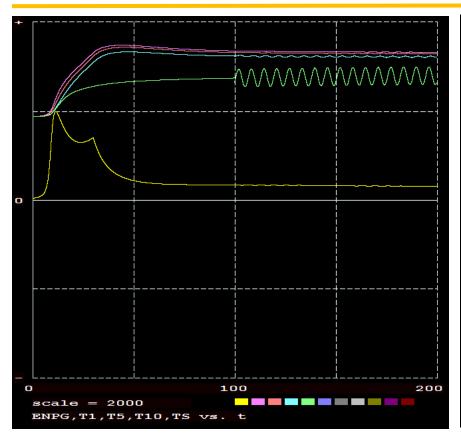


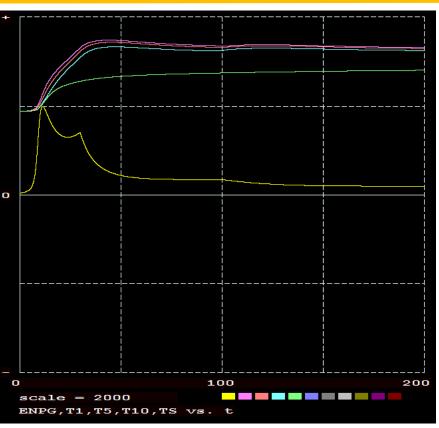
\$0.50 Reactivity Step

100°C Saturation Temperature Step



## **DSS Off-Normal II**



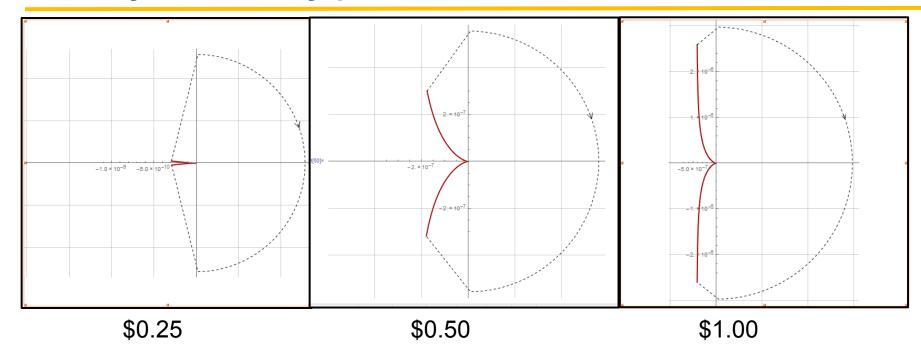


**Temperature Oscillation** 

Loss of Heat Pipe Function



# **Stability Model – Nyquist Plots**



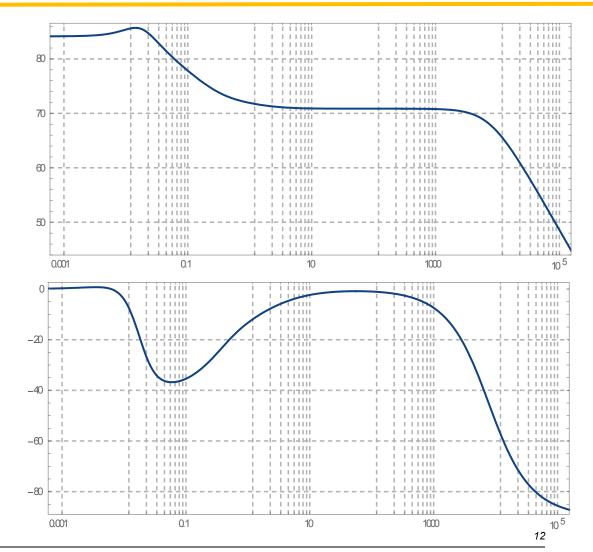
- Higher power results in wider stability margin
- No positive zeros in Open Loop Transfer Function
- Does not encircle -1

Model is unconditional stable in the linear approximation

# **Stability Model – Bode Plots**

Amplitude – Top Frequency – Bottom

- Response is benign
- No discontinuities
- Consistent with Nyquist conclusions

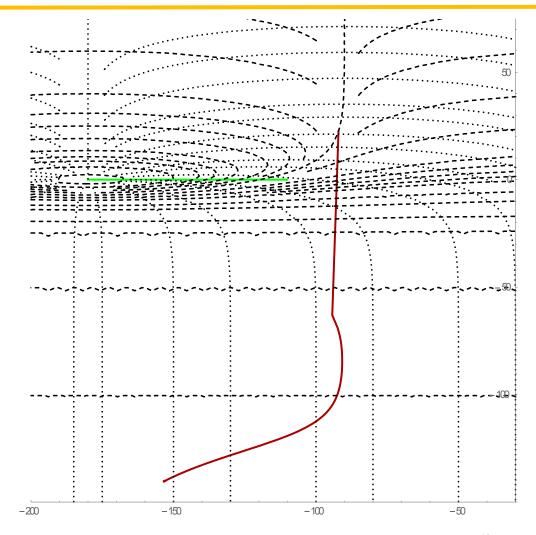






# **Stability Model – Nichols Plot**

- Shows wide stability margin (~75°)
- Result consistent with Nyquist







# **Analysis of Transfer Function Stability**

- Bethe Criteria No infinite resonance in Bode Plots
- Nyquist Criteria Number of clockwise encirclements of 1- plus the number of right hand plane poles is zero (transfer function has not positive poles)
- Nichols Criteria One sheeted full Nichols plot of the transfer function does not intersect the point (-180, 0 db)

These are necessary and sufficient to establish stability of the model in the linear approximation

Bethe criteria is necessary for non-linear system stability



#### **Conclusions and Recommendations**

- Proposed experimental campaign, including zero power critical over full temperature range will minimize uncertainties in important parameters
- Experiments at power will demonstrate system functionality and operability
- Dynamic System model establishes basis for operation and system stability; however, generic heat transfer mechanism used in current model; improvements to be made once experimental data available
- Experimental results may be used to refine model to provide an operational tool

